

# AIAA 96-4245 Analysis of Shuttle Orbiter Reliability and Maintainability Data for Conceptual Studies

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# ANALYSIS OF SHUTTLE ORBITER RELIABILITY AND MAINTAINABILITY DATA FOR CONCEPTUAL STUDIES

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### **ABSTRACT**

In order to provide a basis for estimating the expected support required of new systems during their conceptual design phase, Langley Research Center has recently collected Shuttle Orbiter reliability and maintainability data from the various data base sources at Kennedy Space Center. This information was analyzed to provide benchmarks, trends, and distributions to aid in the analysis of new designs. This paper presents a summation of those results and an initial interpretation of the findings.

# **NOMENCLATURE**

APU	Auxilary Power Unit
COMM	Communications
ECLS	Environmental Control and Life Support
EXP	Exponential
FPOT	Flight Power On Time
GPOT	Ground Power On Time
IOS	Integrated Operations System
IWCS	Integrated Work Control System
HC	Head Count
KSC	Kennedy Space Center
LaRC	Langley Research Center
LOG	Lognormal
LSTAR	Launch + 15 Day Shuttle Trend Analysis
	Report
MHRS	Manhours
MAINT	Maintence
MTAR	Maintenance Trend Analysis Report

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MTBMA	Mean Time Between Maintenance Actions
MTTR	Mean Time To Repair
OMDP	Orbiter Maintenance Down Period
PRACA	Problem Reporting and Corrective Action
PV&D	Purge Vent & Drain
R&M	Reliability and Maintainability
RCM	Reliability Centered Maintenance
RCS	Reaction Control System
SFC/DC	Shop Floor Control/Data Collection
SPDMS	Shuttle Processing Data Management
	System
STS	Space Transportation System
TCS	Thermal Control System
TPS	Thermal Protection System
TVC	Thrust Vector Control
WEIB	Weibull

# INTRODUCTION

One of the best guides for estimating future performance of conceptual systems is current experience with similar systems. For those charged with assessing the support required of future reusable launch systems, the experience base is the Shuttle Orbiter. However, the lack of a suitable compilation of the reliability and maintainability (R&M) history of the Orbiter has been a major hindrance in benefiting from that experience. Such information is needed by those working in space operations who are charged with the responsibility of both assessing the support required of future systems and of identifying the benefits of developing new technologies for support of those systems. This information is used to help establish rational levels of support for a new generation of vehicles that are traceable to current flight experience and to help evaluate the value of new technologies in reducing both the time and cost to operate a new system.

The analysis of aircraft support has used historical R&M data from operational systems in combination with

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simulation models to define and improve the effectiveness of their support systems for over 25 years<sup>1</sup>. Early work defining support for conceptual launch vehicles also attempted to use this approach with discrete event simulation modeling<sup>2-4</sup>. Although useful for launch vehicles in giving general insight to support requirements, the models had to be based on assumed parametric values such as turnaround time, manpower, number of facilities, etc., since historically defined support requirements were generally only available at highly aggregated levels. This level lacked the fidelity necessary to evaluate the effects of introducing new technologies or procedures. For conceptual studies, the modeler is in need of information on the type, frequency and duration of tasks, along with the crew sizes required for support of new launch systems. One of the initial data studies which collected Shuttle support information was specifically designed to aid in the process definition and to define manpower and task times for launch operations<sup>5</sup>. While information from this study aided simulation modeling, it lacked completeness and contained insufficient data to statistically characterize the results.

Lacking good R&M histories on Shuttle, aircraft data has been used to formulate an analysis tool based on parametric estimating relationships<sup>6-8</sup>. This method built on one developed by Weber<sup>9</sup> for analyzing space system designs using aircraft data. As Shuttle data became available in the post Challenger time period, a study by Martin Marietta<sup>10</sup> was initiated to define R&M data from the Shuttle program that was comparable to the aircraft data used by this analysis model. The study provided Shuttle data similar to the aircraft reliability histories, but required major assumptions to develop the maintainability data. A more recent study has confirmed that the maintainability data is not available from the existing Shuttle electronic databases<sup>11</sup> at a fidelity comparable to aircraft databases.

A number of working reports are now being issued to aid those responsible for Shuttle processing. Typical are the MTAR (Maintenance Trend Analysis Report 12), LSTAR (Launch + 15 Day Shuttle Trend Analysis Report Plus 13) and RCM (Reliability-Centered Maintenance 14) reports. The focus of each is on slightly different aspects of the support. Although these reports contain useful modeling information, their emphasis is on process control and are intended to highlight current and emerging problem areas to management attention so that they can be addressed in a timely manner. They do not provide the modeler all of the information nor offer the longer historical perspective needed for use in conceptual studies.

All of these reports are drawn from data contained in the Kennedy Space Center (KSC) data bases. However, none of the cited reports provide a linkage between the problems that initiated maintenance actions and the support manpower and time required to analyze and/or correct it. This is of primary interest for modeling these activities for future launch systems. The recent implementation of the Integrated Work Control System (IWCS) as a part of Shuttle Processing Data Management System (SPDMS) provided the opportunity to define that connection. The Langley Research Center (LaRC) initiated a study by Lockheed Martin Advanced Programs Group<sup>15</sup> at KSC to update the data base that had been developed in 1992<sup>10</sup> and to collect this additional information on maintenance activities which had not been available at the time of the earlier report. The results from this most recent study form the basis of this report. This paper will examine the Shuttle R&M data to identify characteristics and trends consistent with this phase of the program. In particular, it will attempt to provide insight to the manpower and repair time characteristics of the Shuttle's support concept that can be used for modeling the support requirements of future reusable launch vehicles.

# SCOPE/METHODS/APPROACH

Ideally, a complete and detailed component level R&M history would be available for the Shuttle Orbiter, comparable to that available for military aircraft. That level of information, however, is simply not available for Shuttle systems. This study made use of current data collection systems in-place at KSC to collect and analyze information which would be consistent with the level of analysis used in Langley's conceptual studies. Typically, these studies are conducted at the subsystem level. Since these studies are frequently addressing generic technologies and broad-based processing issues, the application of these techniques at the subsystem level is both appropriate and adequate.

The data base presented in this report consists of data records from post-Challenger flights only for the Shuttle Orbiter. Because the focus was on support of reusable elements, the solid rocket motor and external tank data are not shown as a part of this report. The records presented in this paper reflect tasks required for hands-on support of Orbiter processing between flights. It links planned and unplanned work to both the time and workforce required to perform the task. A total of 29 post-Challenger flights are included in the data base and represent over 75,000 support tasks performed over a 4-year period.

The operations processing data maintained at KSC was originally driven by the need to track the status and completion of work. Stand alone data systems were typical until a unified electronic data collection system, the SPDMS II, was implemented after the Challenger accident. IWCS was the latest part of the evolution of this system. In addition to better integrating the standalone systems, the IWCS also provided new software functions that allowed for the first time a limited definition of maintenance requirements based on the historical records. The systems which make up IWCS are the primary source of processing data for this study. These were the Integrated Operating System (IOS), the Shop Floor Control /Data Collection (SFC/DC), and the Problem Reporting and Corrective Action (PRACA) data systems (Figure 1).

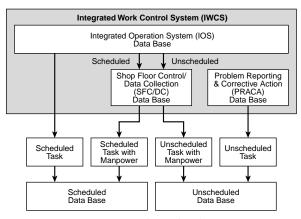


Figure 1. Data base development.

The IOS was used to define both the standard and non-standard tasks for the data base. The standard tasks are frequently referred to as planned or scheduled work. They consists of the Operations and Maintenance Instruction, Repetitive Operations and Maintenance Instruction, Job Card, Work Authorization and the Test Preparation Sheet tasks. The workforce and task time requirements were defined in SFC/DC system for many of the planned tasks identified in the IOS data base. The non-standard or unscheduled tasks were identified in the PRACA data base. These included the Interim Problem Reports, the Problem Reports, and the Discrepancy Reports. Since the PRACA data base does not contain manpower or task time information, it was necessary to use the IOS to identify the corresponding maintenance records in the SFC/ DC data base. Also, because the SFC/DC has been phased into use only in recent years, matching records do not exist for every maintenance action identified in the PRACA data base. For that reason, it became necessary to define the unplanned data from the two different sources. The PRACA data base was used to define the number of maintenance actions and thus the reliability of each subsystem for the purpose of maintenance. The SFC/DC system was used to define the number of people and the time required to perform repair tasks which are then assumed representative of unscheduled maintenance tasks on each subsystem. In a similar fashion, matching records do not exist for every scheduled maintenance task identified in the IOS data base. For that reason, the IOS data base was used to define the number of scheduled tasks and the SFC/DC system was used to define the people and the time required to perform those tasks. Again, these are assumed representative of the scheduled tasks for each subsystem.

Table 1. STS Missions Contained in the R&M Data Base.

		Daia	Base.	
STS#	Mission#	Orbiter	Launch Date	Landing Date
50	48	102	6/25/92	7/9/92
46	49	104	7/31/92	8/8/92
47	50	105	9/12/92	9/20/92
52	51	102	10/22/92	11/1/92
53	52	103	12/2/92	12/9/92
54	53	105	1/13/93	1/19/93
56	54	103	4/8/93	4/17/93
55	55	102	4/26/93	5/6/93
57	56	105	6/21/93	7/1/93
51	57	103	9/12/93	9/22/93
58	58	102	10/18/93	11/1/93
61	59	105	12/2/93	12/13/93
60	60	103	2/3/94	2/11/94
62	61	102	3/4/94	3/18/94
59	62	105	4/9/94	4/20/94
65	63	102	7/8/94	7/23/94
64	64	103	9/9/94	9/20/94
68	65	105	9/30/94	10/11/94
66	66	104	11/3/94	11/14/94
63	67	103	2/3/95	2/11/95
67	68	105	3/2/95	3/18/95
71	69	104	6/27/95	7/7/95
70	70	103	7/13/95	7/22/95
69	71	105	9/7/95	9/18/95
73	72	102	10/20/95	11/5/95
74	73	104	11/12/95	11/20/95
72	74	105	1/11/96	1/20/96
75	75	102	2/22/96	3/9/96
76	76	104	3/22/96	3/31/96

Note: shaded flights not included in this analysis

Table 2. Benchmark R&M Results for Shuttle Subsystems.

			Sched	uled		Unscheduled				
Subsys	Subsys Definition	Number Tasks	Task Time Hours	Maint. Mhrs	Crew Size HC	Maint. Activities		Maint. Mhrs	Crew Size HC	Removal Rate
4	Structures and thermal control	0.4	17.9	45.6	2.2	0.5	9.9	15.9	1.6	20.0%
5	Purge, vent and drain	25.8	23.8	31.5	1.3	20.7	9.6	13.6	1.3	44.0%
6	Thermal control system	33.0	29.5	50.7	1.7	35.1	6.1	9.2	1.5	60.6%
7	Thermal/aerodynamics	1.2	13.7	19.7	1.2	0.2	20.6	20.6	1.0	0.0%
8	Structural dynamics/structures	9.7	18.8	43.0	2.4	27.6	37.7	58.3	1.4	35.9%
9	Thermal protection system (general)	31.6	34.7	71.1	2.0	76.5	16.1	37.4	2.3	13.1%
10 11	Wing (general) Wing leading edge	0.5 1.2	5.4 13.6	10.8 27.9	2.0 2.0	1.2 4.1	7.6 29.8	7.6 47.1	1.0 1.5	4.4% 25.9%
12	Wing box	14.7	9.0	16.1	1.8	1.6	20.1	29.3	1.5	18.8%
13	Elevons	8.8	6.2	11.1	1.7	3.9	12.9	18.1	1.3	29.9%
16	Wing TCS	No Data	0.2		•••	0.4	17.6	35.2	2.0	14.3%
19	Wing TPS	171.5	12.3	22.8	1.9	375.1	15.4	23.0	1.5	28.0%
20	Vertical stabilizer (general)	No Data				No Data				
21	Vertical stabilizer leading edge	3.2	7.6	8.3	1.1	No Data				
22	Vertical fin	14.5	17.4	21.3	1.2	1.9	16.5	18.0	1.1	18.4%
23	Rudder/speed brake	2.4	8.9	11.0	1.2	5.1	47.9	57.4	1.2	23.8%
26	Vertical stabilizer TCS	No Data	7.0	7.0	4.0	No Data	44.7	40.0	4.0	04.00/
29 30	Vertical stabilizer TPS	1.0 1.5	7.3 50.0	7.3 87.1	1.0 1.7	58.2 No Data	11.7	12.3	1.0	21.3%
31	Fuselage (general) Fuselage, upper forward	6.0	76.6	134.8	1.7	4.7	19.1	28.6	1.4	22.3%
32	Fuselage, lower forward	15.4	13.6	17.3	1.1	3.0	18.6	26.1	1.3	23.7%
33	Crew module	59.8	9.7	17.0	1.8	19.3	15.0	19.8	1.3	19.4%
34	Fuselage, mid	39.4	17.1	34.7	2.0	14.2	17.8	29.9	1.6	19.4%
35	Fuselage, aft	83.3	20.1	32.9	1.6	48.0	18.4	22.4	1.2	22.0%
36	Fuselage TCS	No Data				10.8	13.8	20.8	1.4	31.9%
37	Payload bay doors	25.4	11.9	39.8	3.3	7.5	23.5	32.7	1.4	14.1%
38	Fuselage PV&D	No Data				56.2	24.5	26.8	1.2	18.5%
39	Fuselage TPS	5.0	No Data			722.0	20.4	25.8	1.2	17.2%
40	Propulsion/pwr (general)	0.9	20.8	32.9	2.5	No Data	5.2	6.0	1.3	No Data
41 42	Main propulsion Reaction control/TVC	175.7 57.0	19.5 35.3	38.7 44.6	2.0 1.3	85.2 21.9	13.8 16.4	16.5 22.2	1.2 1.2	31.8% 37.5%
43	Orbiter maneuvering	110.7	25.1	38.9	1.6	23.3	11.2	13.5	1.2	25.8%
45	Electrical power generation	16.6	38.8	73.9	1.9	7.4	9.9	11.9	1.2	46.6%
46	Auxiliary power unit	12.5	47.3	68.0	1.4	18.0	20.5	25.0	1.2	49.7%
51	Landing gear	47.4	41.3	93.1	2.2	9.0	10.1	18.3	1.6	26.7%
52	Brake/skid control	6.2	15.0	23.9	1.5	1.95	12.0	16.5	1.4	41.0%
53	Docking mechanism	No Data				1.15	0.6	1.3	2.0	13.0%
54	Payload retention/deployment	15.3	26.4	72.2	2.8	2.9	12.4	21.3	1.9	31.6%
55	Pyrotechnics and range safety	34.8	20.3	33.8	1.7	10.8	9.2	10.9	1.2	50.7%
56	Attachment/separation	18.6	14.1	17.3	1.3	20.3	21.2	23.0	1.1	52.7%
57 50	Aero surface control	0.2	6.3	9.1	1.5	2.8	15.6	15.8 16.0	1.0	12.5%
58 59	Hydraulics Actuation mechanisms	8.7 6.6	51.3 11.5	72.2 16.4	1.4 1.5	26.7 6.1	12.8 19.7	27.8	1.2 1.4	41.4% 29.5%
60	ECLS (general)	5.5	42.3	61.9	1.5	No Data	9.0	12.9	1.4	No Data
61	Atmospheric revitilization	9.4	14.2	19.5	1.3	7.2	16.7	21.9	1.3	34.3%
62	Life support	7.3	22.2	30.3	1.4	7.7	15.7	19.7	1.1	39.9%
63	Active thermal control	14.2	12.7	20.1	1.6	17.2	26.0	37.7	1.7	18.4%
64	Airlock support	2.3	25.7	35.1	1.4	1.9	12.7	14.4	1.2	26.3%
65	Crew provisions	2.0	2.5	2.9	1.2	3.1	17.2	19.3	1.1	44.7%
66	Crew equipment	39.2	23.5	53.4	2.3	37.7	9.6	13.2	1.4	65.2%
70	Avionics (general)	0.2	31.2	43.7	1.2	0.5	0.6	0.6	1.0	30.0%
71 72	Guidance and navigation	8.3	11.0	14.8	1.3	3.1	15.6	18.8	1.2	64.5%
72 73	Data processing	10.7	18.8	24.1	1.3	5.3	13.8	17.0	1.2	80.0%
73 74	Displays and controls	11.0 28.5	10.7 13.2	13.1 24.4	1.2 1.8	16.3	14.8 9.9	17.9 13.2	1.2	76.6% 52.0%
74 75	Communications and tracking Instrumentation (operational)	28.5 44.2	13.2	22.8	2.1	8.8 24.1	9.9 15.9	19.7	1.4 1.2	52.0% 53.6%
75 76	Electrical power distribution	24.0	11.1	21.3	1.9	7.0	17.3	20.2	1.2	66.4%
70 77	Interconnecting wiring	2.4	26.6	57.5	1.8	52.6	13.6	15.8	1.2	19.1%
	Instrumentation development	1.6	16.3	24.7	1.5	0.3	42.4	46.3	1.1	50.0%
78	Instrumentation development									

Mean operating time: GPOT = 1,450 hours; FPOT = 264 hours

The data base presented in this report (Table 1) is drawn from the initial 29 flights minus: the Orbiter Maintenance Down Period (OMDP) flights (STS-53, 66, 73) which were not representative of normal processing; several of the early flights where data collection was initially being implemented (STS-50, 46,47,52); and the last two flights for which all data may not have been available at the time it was downloaded (STS-75, 76). Results for the 20 flights that were included were summarized in terms of the scheduled and unscheduled work required for support for each of the Shuttle's subsystems. These values weighted by the number of tasks are presented as a characterization of the R&M parameters that could be expected using Shuttle technologies for typical missions of similar environments and duration. Representative ground and flight operating hours were developed as a part of the study to be used for defining the maintenance failure rate (Table 2). These rates are not computed here, leaving to the analyst to decide whether the operating hours or some other parameter is the appropriate reliability metric for their study. In addition, histograms were developed for each task to describe the variability in processing time and workforce representative of the task. These were also examined over the 4-year period for trends.

### **RESULTS & DISCUSSION**

# **Summary Results**

A summary of the results are presented in Table 2 for selected Shuttle subsystems. These characteristics are the mean number of scheduled tasks and the mean time and crew size required per task weighted by the number of tasks. Also shown are the mean number of unscheduled maintenance actions for each subsystem along with the mean time to repair and crew sizes used. The removal rate is based on the disposition code for each maintenance action and is also a weighted mean. All results are based on the flight subsystem codes as defined in reference 16. Subsystems that were excluded are those that were not representative of reusable elements such as the external tank, or subsystem codes that describe unique systems such as orbiter experiments or mission kits.

The results are intended to be representative of the frequency of task, the time required and the number of personnel required for touch labor associated with each subsystem. An implicit assumption is made that the type of failures that occur and the time and manpower required for support can be used to uniquely characterize each subsystem code. For example, to maintain a hydraulic system using the same maintenance concept as Shuttle would require 8.7 tasks after each flight using sufficient personnel to average a crew size of 1.4 working 51.3 hours on each task. In addition, the number of unscheduled maintenance actions that could be expected for a new system flying a similar technology in the same flight environment would be 26.7. An average crew of 1.2 could perform repair in 12.8 hours for each maintenance action required. These task/repair times are based on the assumption that the data collected from the SFC/DC were representative of all tasks for each subsystem. Accounting for new technology, changes in the operating environment, or alternate processing procedures for future launch systems would be accomplished by the modeler based on these benchmark values.

Not all scheduled tasks could be identified by subsystem code in the IOS data base, resulting in an underestimate of the total number of tasks required. The task/ repair times presented here represent the time from task assignment to close-out including accessing, diagnosing, and some short term delays. Delays that were coded into the shop floor data have been excluded from the serial time required for the task. The original data records contained some tasks that were never closed. These were assumed to be procedural errors and a task time of 12 hours was assigned to these. This is the longest a technician could typically work in a day even with overtime. It should be noted that the Main Propulsion subsystem data generally includes only the work required to remove and replace the engines after each flight. The actual engine repair work is accomplished in a repair shop which is not a part of the SFC system. That data was not available for this study. It also must be noted that no data entry against a subsystem does not necessarily indicate that no work was required. Since the data system has been phased in, work may have been accomplished before the data system was instituted. Also since the number of tasks are from a different data base than the one in which the maintenance work was defined, a certain amount of inconsistency is inevitable. In addition, it appears that the assignment of the subsystem to the work performed could be done independently in the various data bases, so at times this identification was redefined to different subsystems.

Several subsystems were selected to be representative of different types of support: thermal protection, propulsion, power, hydraulics, avionics and electrical. The data for each were examined for any observable trends over the time period covered by the data and for distribu-

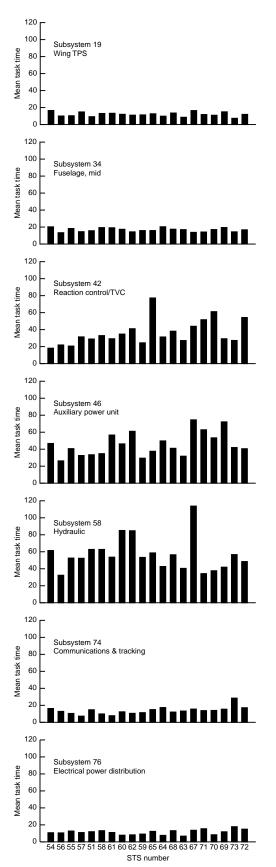


Figure 2. Scheduled mean task time per mission.

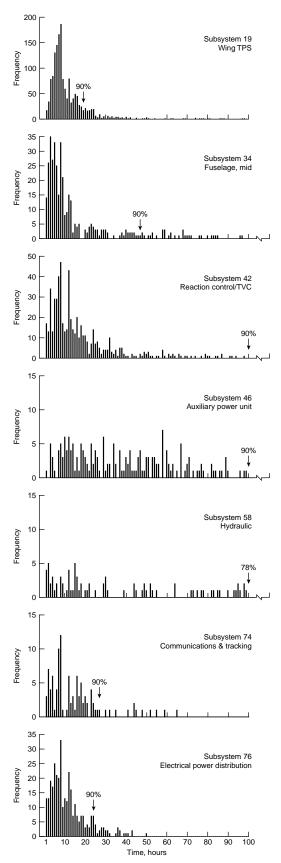


Figure 3. Scheduled mean task time frequency distribution.

Table 3. Results of Curve Fitting for Scheduled Task Times.

Subsystem	n	Sample mean	Sample std dev	R <sup>2</sup> exponential	R <sup>2</sup> Weibull	R <sup>2</sup> normal	R <sup>2</sup> lognormal	Best fit
Wing TPS	380	17.06	23.83	62	86	44	88	Log/Weib
Fuselage, mid	388	16.25	23.83	88	94	66	95	Log/Weib
RCS	380	40.37	18.63	55	93	47	96	Log/Weib
APU	211	47.33	42.05	98	94	84	87	Exp/Weib
Hydraulics	104	51.82	46.56	90	92	89	80	Weib/Exp
Comm/Tracking	339	13.22	14.69	96	98.5	72	94	Weib/Exp
Electrical	333	11.35	9.30	98	97	86	90	Exp/Weib

Table 4. Results of Curve Fitting for Unscheduled Repair Times.

Subsystem	n	Sample mean	Sample std dev	R <sup>2</sup> exponential	R <sup>2</sup> Weibull	R <sup>2</sup> normal	R <sup>2</sup> lognormal	Best fit
Wing TPS	137	15.36	19.80	86	96	63	96	Log/Weib
Fuselage, mid	119	16.89	34.87	34	97	39	96	Weib/Log
RCS	37	16.50	24.92	65	96	55	94	Weib/Log
APU	79	20.75	25.82	86	97	70	91	Weib/Log
Hydraulics	197	13.00	14.11	96	99	74	94	Weib/Exp
Comm/Tracking	43	9.86	7.57	96	97	91	96	Weib/Log
Electrical	63	17.30	19.55	96	95	74	99	Log/Exp

tion of their task time requirements. The results are presented for the scheduled support in Figures 2 and 3 and Table 3, and for the unscheduled in Figure 4 and Table 4.

# Scheduled

For scheduled support, the mean task times by mission are shown in Figure 2 for the representative subsystems. These are presented as a function of the STS flights plotted in order of their mission sequence. For most of these systems, no task time trend could be observed. A decreasing trend might be expected for repetitive tasks such as these. The reason this is not observed could be attributed to several factors. It may be that any learning that takes place is offset by increasing difficulties in performing the task due to aging equipment, both airborne and ground. Also the fixed flight schedule, limiting the fleet to seven flights per year places no incentive on reducing the time required for a task as long as it is within the time allotted to support the flight rate. And finally, the nature of the task may be changing over time with the procedures being redefined to accommodate new information. The assumption is made that the support task functions are consistently the same between flights. The mean task times show mechanical type systems such as the Hydraulics, Auxiliary Power Unit (APU) and Reaction Control System (RCS) require significantly longer work times than do the avionics, electrical and Thermal Protection System (TPS).

The task time frequency distributions are shown in Figure 3 for each system. Curve fitting the data, most systems display a lognormal or Weibull distribution for the scheduled task times. These results are summarized in table 3 for samples from each representative subsystem. The APU and Electrical subsystems also display a very good fit to an exponential distribution. The results shown in Figure 3 also illustrate the longer work times required of the mechanical systems with larger means and standard deviations than the other systems. These distributions are shown for up to 100 hours of time to complete a task. Half of the tasks are completed in a single work shift for the TPS, Mid Fuselage, Communications & Tracking and Electrical Power Distribution subsystems. All except the Hydraulics and the RCS systems complete 90 percent of the tasks within that period. The Hydraulics system completes only 78 percent of the tasks within that time. The multishift tasks appear to be characteristic of the scheduled support for these systems.

### Unscheduled

The number of maintenance actions and the distribution of task times are shown for the unscheduled repair tasks in Figure 4. Most of these systems can complete

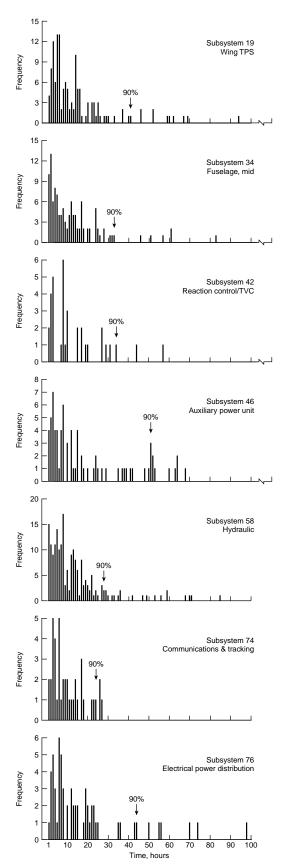


Figure 4. Unscheduled repair time frequency distribution.

half of the task within a single shift and all are 90 percent complete within 7 shifts (56 hours). The probability distribution for the subsystem repair time can be modeled accurately, in most cases, as either a Weibull or lognormal distribution with the parameter values as shown in Table 4. The fact that either distribution may be used in all but the hydraulics or electrical subsystem is not surprising since both distributions can take on similar shapes. Historically the lognormal distribution has been used to model repair times. The repair time of hydraulics and electrical subsystems may also be modeled as an exponential distribution. The use of the exponential distribution is further supported by the fact that the sample mean and standard deviation are "close" to each other. Theoretically they have the same value. Since the exponential distribution is also a special case of the Weibull (when the shape parameter equals one), then the fact that the Weibull is also a good fit is expected.

In order to identify a distribution for the number of failures per mission, the chi-square goodness-of-fit test was applied to three discrete distributions: the binomial, Poisson, and negative binomial. In all cases, the negative binomial was the only acceptable fit with the parameter values as shown in Table 5. However, for the Wing TPS, the large chi-square value indicates the fit was marginal. This result is consistent with aircraft modeling in which the negative binomial has been used to represent the number of demands (i.e. failures) per 100 flying hours. The negative binomial has a variance-tomean ratio greater than one (the Poisson equals one and the binomial is less than one). Aircraft data and the Shuttle data for the seven subsystems analyzed have shown a variance-to-mean ratio greater than one. Therefore, this result is not surprising.

In simulating a space transportation system, the above results can be used to randomly determine the number of unscheduled maintenance actions to be expected for each subsystem following a mission. Then, by simulating each maintenance action, a random draw from the fitted repair time distribution will be made to determine a simulated repair time. With the proper identification of crew sizes, and by constraining the number of crews available each shift, a realistic vehicle turntime and mission rate can then be obtained from the simulation model.

Subsystem reliability, like component maintenance reliability, is based on the amount of time or cycles that the system successfully functions over its operating life. Representative operating hours were developed as a part of the study to be used for defining the maintenance fail-

Table 5. Results of Curve Fitting for Number of Failures per Mission.

Subsystem	Best fit	Chi-sq stat	Parameter s	Parameter p	Mean	Std dev
Wing TPS	Neg Bin	41.745	4	.01	375.0	178.60
Fuselage, mid	Neg Bin	1.753	5	.26	14.2	7.16
RCS	Neg Bin	2.747	5	.18	21.85	10.80
APU	Neg Bin	2.590	3	.14	18.0	10.14
Hydraulics	Neg Bin	2.789	7	.21	26.7	10.85
Comm/Tracking	Neg Bin	1.106	2	.19	8.75	6.46
Electrical	Neg Bin	1.066	4	.36	7.0	4.28

Negative binomial density function:  $f(x) = {s+x-1 \choose x} p^X (1-p)^X$ ; x = 0,1,2,3...

Table 6. Power-on Values

Description %-on hrs  Purge, vent, and drain 8 1  Payload bay doors 3 1  Fuselage PV&D 8 0  Main propulsion 24 1  Reaction control/TVC 37 FPOT  Electrical power generation 6 FPOT  Auxiliary power unit 24 4  Fyortechnics and range safety 5 1  Aero surface control 4 4  Hydraulics 12 4  Cells (general) (see also dependency desc for payload) 14 FPOT  Active thermal control 100 FPOT  Avionics (general) (see also dependency desc for payload) 100 FPOT  Avionics (general) (see also dependency desc for payload) 100 FPOT  Guidance and navigation 14 FPOT  Guidance and navigation 14 FPOT  Data processing 100 FPOT  Jisplays and controls 100 FPOT  Communications and tracking 14 FPOT  Instrumentation (operational) 100 FPOT		Table 6. Power-on Val	ues.	
5 Purge, vent, and drain 37 Payload bay doors 3 1 38 Fuselage PV&D 8 0 41 Main propulsion 24 1 42 Reaction control/TVC 37 FPOT 45 Electrical power generation 6 FPOT 46 Auxiliary power unit 24 4 55 Pyrotechnics and range safety 5 1 57 Aero surface control 4 4 58 Hydraulics 12 4 59 Actuation mechanisms 14 4 60 ECLS (general) (see also dependency desc for payload) 14 FPOT 61 Atmospheric revitalization 100 FPOT 62 Life support 17 FPOT 63 Active thermal control 100 FPOT 64 Airlock support 14 0 70 Avionics (general) (see also dependency desc for payload) 100 FPOT 71 Guidance and navigation 14 FPOT 72 Data processing 100 FPOT 73 Displays and controls 100 FPOT 74 Communications and tracking 14 FPOT 75 Instrumentation (operational) 100 FPOT		Subsystem	GPOT,	FPOT,
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41 Main propulsion 24 1 42 Reaction control/TVC 37 FPOT 45 Electrical power generation 6 FPOT 46 Auxiliary power unit 24 4 55 Pyrotechnics and range safety 5 1 57 Aero surface control 4 4 58 Hydraulics 12 4 59 Actuation mechanisms 14 4 60 ECLS (general) (see also dependency desc for payload) 14 FPOT 61 Atmospheric revitalization 100 FPOT 62 Life support 17 FPOT 63 Active thermal control 100 FPOT 64 Airlock support 14 0 70 Avionics (general) (see also dependency desc for payload) 100 FPOT 71 Guidance and navigation 14 FPOT 72 Data processing 100 FPOT 73 Displays and controls 100 FPOT 74 Communications and tracking 14 FPOT 75 Instrumentation (operational) 100 FPOT	37	Payload bay doors	3	1
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dependency desc for payload)  61 Atmospheric revitalization  62 Life support  63 Active thermal control  64 Airlock support  70 Avionics (general) (see also dependency desc for payload)  71 Guidance and navigation  72 Data processing  73 Displays and controls  74 Communications and tracking  75 Instrumentation (operational)  100 FPOT  110 FPOT  120 FPOT  131 FPOT  141 FPOT  152 Instrumentation (operational)	59	Actuation mechanisms	14	4
61 Atmospheric revitalization 100 FPOT 62 Life support 17 FPOT 63 Active thermal control 100 FPOT 64 Airlock support 14 0 70 Avionics (general) (see also dependency desc for payload) 100 FPOT 71 Guidance and navigation 14 FPOT 72 Data processing 100 FPOT 73 Displays and controls 100 FPOT 74 Communications and tracking 14 FPOT 75 Instrumentation (operational) 100 FPOT	60	ECLS (general) (see also		
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77 Interconnecting wiring 100 FPOT	77	Interconnecting wiring	100	FPOT
79 Flight control 12 1	79	Flight control	12	1
91 Primary avionics system software 100 FPOT	91	Primary avionics system software	100	FPOT
92 Backup flight system software 100 FPOT	92	Backup flight system software	100	FPOT
93 SSME software 24 1	93	SSME software	24	1
95 Test controller supervisor software 100 0	95	Test controller supervisor software	100	0
96 General purpose computer – initial	96	General purpose computer – initial		
program load software 100 FPOT		program load software	100	FPOT

ure rate. The mean Ground Power On Time (GPOT) and Flight Power On Time (FPOT) for the 20 missions analyzed is 1,450 and 264 hours respectively, as summarized in Table 2. For those systems where the power-on time was considered relevant to maintenance reliability of the system, the percentage of operating hours when the systems were being serviced on the ground were developed. This was done by Lockheed in consultation with the Test Project Engineers and are shown in Table 6 for each subsystem. Also, the amount of the mission time is defined along with specific operating hours for subsystems that were not dependent on mission length. This information can then be used to compute the mean time between maintenance actions (MTBMA) required for these subsystems. These rates are not computed here, leaving to the analyst to decide whether the operating hours or some other parameter such as cycles is the appropriate reliability metric for their study.

A comparison of both scheduled and unscheduled work leads one to several characteristics of this support. In general, the number of scheduled tasks will be equal to or greater than the number of unscheduled tasks. Also, for the representative cases, scheduled tasks times for the mechanical systems are more than twice the mean unscheduled repair times for those same systems, and for Hydraulics it is four times the mean repair time. All other systems have consistent task times whether for scheduled or unscheduled work. Task time distributions for both appear to be primarily Weibull or lognormal.

# SUMMARY/CONCLUSIONS

The Shuttle support data collection system at KSC was established for the purpose of accounting for system and element processing requirements. Although not established to support R&M data analysis, much of the

information is relevant to reusable launch vehicles and was used to form a Shuttle R&M data base. This paper is a preliminary report on the analysis of that information. The data is used to characterize the R&M support for subsystems on future reusable launch vehicles on the assumption that it is representative of the support required for each subsystem. The results presented provide benchmark values of repair rates, manpower and task times that can be used by the analyst for guidance in allocating both reliability and maintainability of new systems based on the flight experience of the Shuttle Orbiter. The results of analysis for shape distribution are also presented for seven representative types of support including thermal protection, mechanical systems, avionics, electrical distribution and power. These results represent the first analysis of maintenance support for the Shuttle subsystems based on previously unavailable historical manpower records.

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